

## Bézier curves

### History

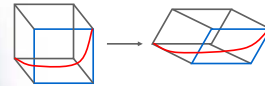
- Renault car design, '60s
- First practical mathematical model for curves used in design
- Replaced point sets, physical models, and French curves in design
- Could be used for numerical milling machines



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## Bézier curves

- Based on the idea of cube deformation (to parallelepiped)

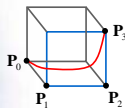


- Embedded cubic curve to opposite corners, tangential to edges, is unique

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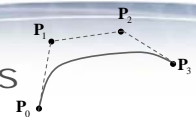
## Bézier curves

- Control points  $P_0, P_1, P_2, P_3$  determine deformations and hence determine the curve



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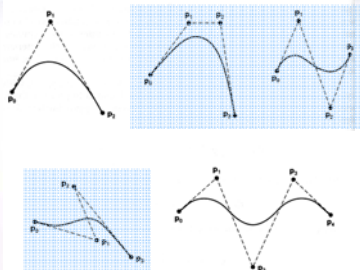
## Cubic Bézier curves



- Determined by 4 control points  $P_0, P_1, P_2, P_3$
- Contained in convex hull of control polygon
- End points of curve interpolate (touch)  $P_0$  and  $P_3$
- End of curves tangent to  $P_1 - P_0$  and  $P_3 - P_2$
- Curve 'mimicks' control polygon

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## Some Bézier curves



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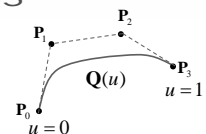
## Bézier curves

- Formal definition:

$$Q(u) = \sum_{j=0}^3 P_j B_j(u)$$

$$0 \leq u \leq 1$$

- Weighted average of control points
- Note:  $Q, P$  are vectors,  $B$  is a scalar



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## Bézier curves

$$Q(u) = \sum_{i=0}^3 P_i B_i(u)$$

- Weight functions are called blending or basis functions. Sum of weights is always 1
- With Bézier curves, the weights are cubic Bernstein functions:

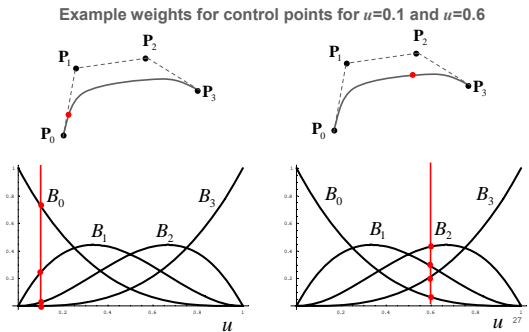
$$B_0(u) = (1-u)^3$$

$$B_1(u) = 3u(1-u)^2$$

$$B_2(u) = 3u^2(1-u)$$

$$B_3(u) = u^3$$

## Bézier curves $Q(u) = \sum_{i=0}^3 P_i B_i(u)$



## Exercise

- Draw the 2D Bézier curve with control points
  - $P_0 = P_3 = (0,0)$
  - $P_1 = (1,0)$
  - $P_2 = (1,1)$

## Solution

$$Q(u) = 3u(1-u)^2 \begin{pmatrix} 1 \\ 0 \end{pmatrix} + 3u^2(1-u) \begin{pmatrix} 1 \\ 1 \end{pmatrix} = \begin{pmatrix} 3u(1-u)^2 + 3u^2(1-u) \\ 3u^2(1-u) \end{pmatrix}$$

## Bézier curves

- Because each point on the curve is a weighted average of the control points, the curve cannot leave the convex hull of the control polygon
- Except at the end points, all weights are non-zero  $\rightarrow$  moving a control point affects the entire curve. (No local control)

## Bézier curves: matrix form

$$Q(u) = \sum_{i=0}^3 P_i B_i(u) \text{ Expands to}$$

$$Q(u) = P_0(1-u)^3 + P_1 3u(1-u)^2 + P_2 3u^2(1-u) + P_3 u^3$$

Which is often found in the matrix form

$$Q(u) = \mathbf{U} B_z \mathbf{P}$$

$$= \begin{bmatrix} u^3 & u^2 & u & 1 \end{bmatrix} \begin{bmatrix} -1 & 3 & -3 & 1 \\ 3 & -6 & 3 & 0 \\ -3 & 3 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} P_0 \\ P_1 \\ P_2 \\ P_3 \end{bmatrix}$$

Note the 'incorrect' notation, treating the P as scalars

## Bézier curves

- General Bézier curves (not only cubic), with  $d+1$  control points  $\mathbf{P}_i$

$$\mathbf{Q}(u) = \sum_{i=0}^d \mathbf{P}_i B_i^d(u)$$

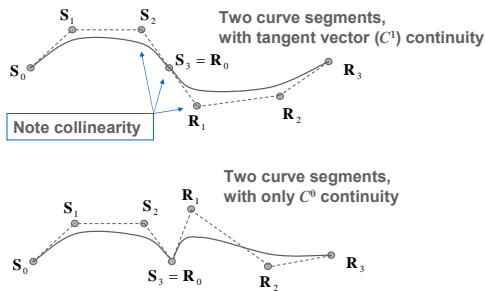
$$B_i^d(t) = \binom{d}{i} t^i (1-t)^{d-i}$$

where  $\binom{d}{i} = \frac{d!}{i!(d-i)!}$ <sup>32</sup>

## Joining Bézier curves

- A four-control-point curve is too small for most applications  $\rightarrow$  join multiple curves
- Usually requires smoothness constraint at joints

## Joining Bézier curves



## Joining Bézier curves

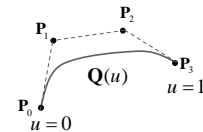
- Bézier curves are tangent to the control polygon at the begin and end:

$$\mathbf{Q}(u) = \mathbf{P}_0(1-u)^3 + \mathbf{P}_1 3u(1-u)^2 + \mathbf{P}_2 3u^2(1-u) + \mathbf{P}_3 u^3$$

$$\mathbf{Q}'(u) = -\mathbf{P}_0 3(1-u)^2 + \mathbf{P}_1 3(1-u)^2 - \mathbf{P}_1 6u(1-u) + \mathbf{P}_2 6u(1-u) - \mathbf{P}_2 3u^2 + \mathbf{P}_3 3u^2$$

$$\mathbf{Q}'(0) = 3(\mathbf{P}_1 - \mathbf{P}_0)$$

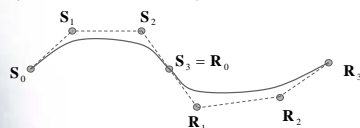
$$\mathbf{Q}'(1) = 3(\mathbf{P}_3 - \mathbf{P}_2)$$



## Joining Bézier curves

- For a  $C^1$  joint, the tangent vectors on either side must match

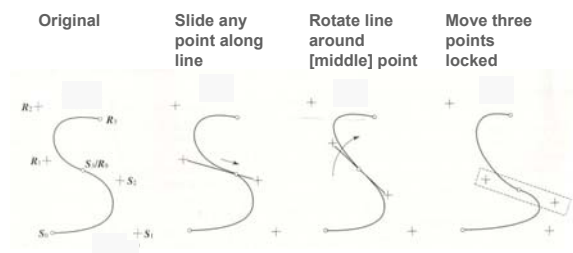
$$\mathbf{S}_3 - \mathbf{S}_2 = k(\mathbf{R}_1 - \mathbf{R}_0)$$



- i.e. the three control points near a joint must be in a line

## Joining Bézier curves

Three options to maintain  $C^1$  continuity when editing



Often very cumbersome/restrictive in practice!<sup>37</sup>

### Bézier curves: summary

- Polynomial curve, often of degree 3
- Shape 'mimicks' control polygon
- No local control
- First and last control point touched
- Tangent to first and last control edge
- Curve is invariant (retains shape) under affine transformation of control points

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### Bézier curves: summary

- Some drawbacks of Bézier curves:
  - No local control
  - Maintaining  $C^1$  continuity of joint segments requires constraints
  - Number of control points ( $d$ ) determines the degree of the curve ( $d-1$ )

These can be overcome by using B-spline curves

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### B-spline curves

- A *spline* is
  1. a thin wood or metal strip (used in building construction)
  2. a piecewise polynomial curve
- A B-spline curve
  - does not (in general) pass through its control points
  - is a piecewise polynomial (mostly cubic)
  - can have any number of segments
  - depends only on local control points

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### B-spline curves

- General formulation: weighted combination of control points ( $\mathbf{P}$ ):
 
$$\mathbf{Q}(u) = \sum_{k=0}^n \mathbf{P}_k B_{k,d}(u) \quad \begin{matrix} u_{\min} \leq u \leq u_{\max} \\ 2 \leq d \leq n+1 \end{matrix}$$

$n+1$	# control points
$d-1$	degree of polynomials ( $d=4$ for cubic)
$B$	blending functions

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## Cubic B-spline curves

- cubic splines ( $d=4$ ):

$$\mathbf{Q}(u) = \sum_{k=0}^n \mathbf{P}_k B_{k,4}(u) \quad \text{Entire curve} \quad u_{\min} \leq u \leq u_{\max}$$

$$\mathbf{Q}_i(u) = \sum_{k=0}^3 \mathbf{P}_{i-3+k} B_{i-3+k}(u) \quad \text{Local variant (used by Watt) for segment } i \quad 0 \leq u \leq 1$$

$$\mathbf{Q}_i(u) = \mathbf{U} \mathbf{B}_s \mathbf{P}$$

$$= \begin{bmatrix} u^3 & u^2 & u & 1 \end{bmatrix} \frac{1}{6} \begin{bmatrix} -1 & 3 & -3 & 1 \\ 3 & -6 & 3 & 0 \\ -3 & 0 & 3 & 0 \\ 1 & 4 & 1 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{P}_{i-3} \\ \mathbf{P}_{i-2} \\ \mathbf{P}_{i-1} \\ \mathbf{P}_i \end{bmatrix}$$

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## Cubic B-splines

$$\mathbf{Q}_i(u) = \sum_{k=0}^3 \mathbf{P}_{i-3+k} B_{i-3+k}(u)$$

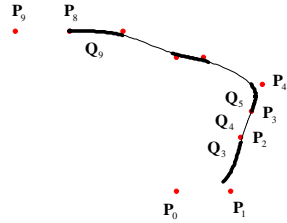
First segment is  $\mathbf{Q}_3$ .  
 $\mathbf{Q}_3$  depends on  $\mathbf{P}_0 \dots \mathbf{P}_3$

The diagram shows a sequence of control points  $\mathbf{P}_0, \mathbf{P}_1, \mathbf{P}_2, \mathbf{P}_3, \mathbf{P}_4$  represented as red dots. A curve segment labeled  $\mathbf{Q}_3$  is shown passing through the points  $\mathbf{P}_1$  and  $\mathbf{P}_2$ . The curve is concave up between  $\mathbf{P}_1$  and  $\mathbf{P}_2$ .

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## Cubic B-splines

$$Q_i(u) = \sum_{k=0}^3 P_{i-3+k} B_{i-3+k}(u)$$

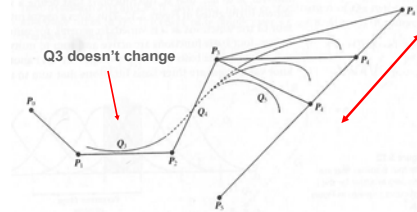


- Each segment  $Q_i$  depends on four control points
- # segments = (# control points) - 2
- In general no end point interpolation
- Blending functions are  $C^2$  continuous  $\rightarrow$  so is  $Q$  (linear combination of  $B$ s)

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## Cubic B-splines

- Since each point of the curve depends on four control points only, we have local control

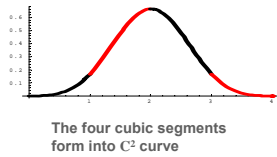
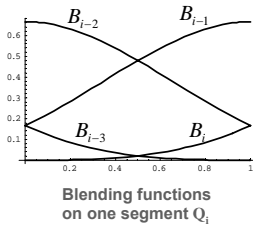


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## Uniform Cubic B-splines

$$Q_i(u) = \sum_{k=0}^3 P_{i-3+k} B_{i-3+k}(u)$$

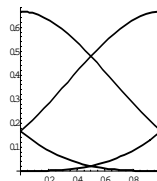
- **Uniform** B spline: the blending functions are all identical



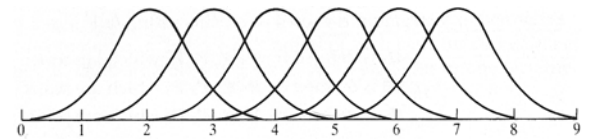
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## Uniform Cubic B-splines

$$Q_i(u) = \sum_{k=0}^3 P_{i-3+k} B_{i-3+k}(u)$$



- Repetition of the blending function gives all the weights for the entire curve
- Now note that why the '-3' is in the formula for  $Q_i$ : only from  $u=3$  are there four functions active, and the sum of weights=1

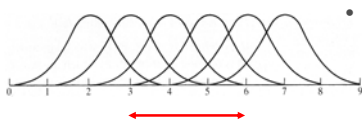


## Uniform Cubic B-splines

- The entire curve:

$$Q(u) = \sum_{k=0}^n P_k B_{k,4}(u) \quad u_{\min} \leq u \leq u_{\max}$$

- $u_{\min}$  and  $u_{\max}$  are determined by the range of  $u$  where there are four blending functions active.
- Values for  $B$  come from shifting the standard  $B$



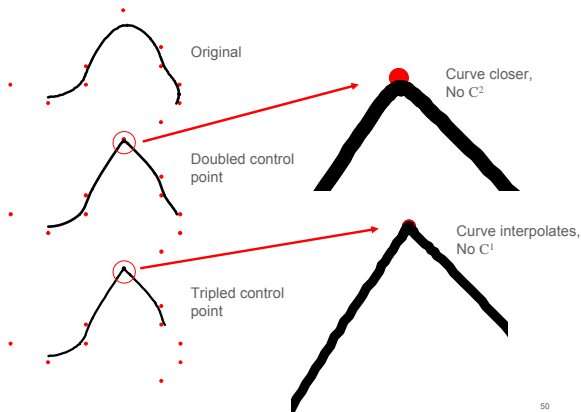
- e.g.  $3 \leq u \leq 6$  for 5 control points

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## Uniform Cubic B-splines

- In general, B-splines do not interpolate (touch) points
- Doubling a control point draws the curve nearer
- Tripling a control point forces interpolation
- Theoretically, the curve is still  $C^2$ , but the geometric continuity is reduced.

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## Non-uniform B-splines

- A better way than control point duplication is to specify where blending functions (bf) have to start
- **Knot** = A start or end point of a bf
- **Knot vector** = Collection of all knots
- By using knots, we can enforce there are always 4 bf active → end and mid point interpolation possible
- bf need to be rewritten (to retain sum=1 and other properties). Each (cubic) bf is determined by a group of 5 knots

### Example: end point interpolation

- With 6 control points, the normal knot vector  $u_i$  with uniform B-splines is  $[0, 1, 2, 3, 4, 5, 6, 7, 8, 9]$  and  $3 \leq u \leq 6$

$$Q(u) = \sum_{k=0}^5 P_k B_{k,4}(u)$$

(Because six control points means  $B_0 \dots B_5$  start at  $u=0, 1, 2, 3, 4, 5$ , and at  $u=6, 7, 8, 9$  bf end)

$[0, 1, 2, 3, 4, 5, 6, 7, 8, 9]$   
 Determines shape of  $B_0$   
 Determines shape of  $B_1$   
 Etc.

Since 5 points are needed for each bf, we need a knot vector of length 9 for 6 control points

### Example (cont.)

$$Q(u) = \sum_{k=0}^5 P_k B_{k,4}(u)$$

- We now change the knot vector (of 9 entries) such that 4 bf start at the first control point, and 4 end at the last, so the end points are interpolated

$[0, 0, 0, 0, 1, 2, 3, 3, 3, 3]$

Determines shape of  $B_0$   
 Determines shape of  $B_1$   
 Etc.

### Non-uniform B-splines: Generating the Blending functions

$$Q(u) = \sum_{k=0}^n P_k B_{k,d}(u)$$

- Cox-De Boor recursive algorithm

$$B_{i,1}(u) = \begin{cases} 1 & u_i \leq u \leq u_{i+1} \\ 0 & \text{otherwise} \end{cases}$$

$$B_{i,d}(u) = \frac{u - u_i}{u_{i+d-1} - u_i} B_{i,d-1}(u) + \frac{u_{i+d} - u}{u_{i+d} - u_{i+1}} B_{i+1,d-1}(u)$$

- With knot vector  $[u_i]$ , degree  $d-1$
- $x/0$  is defined 0